


IFE/KR/E-2014/001



Overview of Halden
Reactor LOCA
experiments (with
emphasis on fuel
fragmentation) and plans



Institute for Energy Technology



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| Report title Overview of Halden Reactor LOCA experiments (with emphasis on fuel fragmentation) and plans | | | |
| Summary <p>The U.S. Nuclear Regulatory Commission (NRC) is a member of the OECD Halden Reactor Project and is participating in the joint programme of LOCA experiments in the Halden Reactor. The presentation “Overview of Halden Reactor LOCA Experiments and plans” by B. Oberlander and W. Wiesenack was given at the United States Nuclear Regulatory Commission (US_NRC) Public Meeting on Fuel Fragmentation, Relocation and Dispersal - in Rockville, MD, USA on March 13-14, 2014. The presentation has the US-NRC document no. ML14071A197 in http://meetings.nrc.gov/pmns/mtg?do=details&Code=20140319</p> <p>NRC Public Meeting / Public hearing on on “fuel fragmentation, relocation and dispersal under Loss-of-Coolant Accident (LOCA) conditions”. The U.S. Nuclear Regulatory Commission staff is performing additional research and analysis on fuel fragmentation, relocation and dispersal under Loss-of-Coolant Accident (LOCA) conditions and is soliciting relevant input from interested parties on various technical issues associated with this subject. The purpose of this meeting is to have technical discussions and an information exchange related to research on fuel fragmentation, relocation and dispersal under LOCA conditions. Various potential approaches to regulatory resolution of fuel fragmentation, relocation and dispersal under LOCA conditions will also be discussed. The potential implications of the research findings to the analysis of non-LOCA events that result in fuel rod rupture will also be discussed. Stakeholders from industry, research institutes, licensees and utilities, regulatory agencies, both domestic and international, and other interested public stakeholders are encouraged to participate in the meeting.</p> | | | |
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1 Introduction

The U.S. Nuclear Regulatory Commission (NRC) is a member of the OECD Halden Reactor Project and is participating in the joint programme of LOCA experiments in the Halden Reactor. The presentation “Overview of Halden Reactor LOCA Experiments and plans” by B. Oberlander and W. Wiesenack was given at the United States Nuclear Regulatory Commission (US_NRC) Public Meeting on Fuel Fragmentation, Relocation and Dispersal - in Rockville, MD, USA on March 13-14, 2014. The presentation has the US-NRC document no. ML14071A197 in

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2 Presentation

2.1 HRP IFA-650 LOCA test series – Objectives

The Halden Reactor Project LOCA testing started about ten years ago with a workshop and a group of experts defining the objectives. They identified

- fuel fragmentation, relocation and dispersal

as one of the major issues of high burnup fuel behaviour in a LOCA. This has been the main focus of the test series after the execution of IFA-650.4 which showed considerable fuel fragmentation and dispersal. The presentation will mainly summarise the results related to these issues.

HRP IFA-650 LOCA test series

– Objectives –

Covered by this presentation:

- **Fuel fragmentation, relocation and dispersal**
 - Tests have concentrated on these issues after IFA-650.4 which showed considerable fuel fragmentation and dispersal

Not addressed in this presentation:

- Cladding overheating and oxidation due to fuel relocation
- Secondary transient hydriding near the burst region
- Release of iodine and caesium

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Figure 1 HRP IFA-650 LOCA test series – Objectives

The other objectives are not particularly addressed in this presentation:

- Cladding overheating and oxidation due to fuel relocation
- Secondary transient hydriding near the burst region

With respect to these objectives, PIE was done on some segments subjected to LOCA conditions in the test series.

- Release of iodine and caesium

The release of the radioactive fission products iodine and caesium was measured in several tests. The results are not reported in this presentation, but it can be said that the release was found to be lower than usually assumed in safety assessments.

2.2 Tests carried out

The table gives an overview of the tests carried out so far. They comprise five tests with PWR fuel, four tests with BWR fuel, and two with VVER fuel, all using high burnup fuel segments from commercial irradiations. Important parameters are burnup from 44 to 92 MWd/kg, cladding oxide thickness and the related hydrogen content which influence cladding

Tests carried out

| | 1,2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 |
|----------------------------------|-----|-------------------|-------------------|-------------------|---------------|---------------|---|-------------------|---------------|---------------|---------------|---------------|---------------|
| Target PCT (°C) | | 800 | 800 | 1100 | 850 | 1100 | | 1100 | 850 | 1000 | 850 | 870 | 850 |
| Fuel type | | PWR | PWR | PWR | VVER | BWR | | PWR | PWR | VVER | BWR | BWR | BWR |
| Rod ident. | | V1-515/3 | 14D/7 | V1-515/7 | J13 | AEB-070-E4 | | 14D/3 | F08/3 | J13/3 | AEB 072-E4 | AEB 072-4C | AEB 072-J9 |
| Span no. | | 2-3 | 5-6 | 5-6 | --- | 3 | | 2-3 | 3 | --- | 3 | | |
| Fuel length (cm) | | 48 | 48 | 48 | 48 | 47 | | 48 | 44 | 48 | 38 | 38 | 36 |
| Cycles | | 6 | 7 | 6 | 4 | 3 | | 7 | 6 | 4 | 5 | 7 | 7 |
| Burnup (MWd/kgU) | | 81.9 | 92.3 | 83.4 | 55.5 | 44.3 | | 89.9 | 61.0 | 56.0 | 72.3 | 74.1 | 70.8 |
| Oxide thickness (µm) | | 18-27 | 10 | 65 | ~5 | <10 | | 7-8 | 20-30 | ~5 | 40 | 20 | |
| Hydrogen, ppm | | 250 | 50 | 650 | 100 | 44 | | 30 | 150-220 | 100 | 300 | 300 | |
| Cladding | | Zry-4/ 1.47%Sn | Zry-4/ 1.47%Sn | Zry-4/ 1.47%Sn | E110 | LK3/L | | Zry-4/ 1.47%Sn | Zry-4 | E110 | LK3/L | LK3/L | LK3/L |
| D _{out} /thickness (mm) | | 10.75/ 0.725 | 10.75/ 0.725 | 10.75/ 0.725 | 9.13/ 0.68 | 9.62/ 0.63 | | 10.75/ 0.725 | 9.50/ 0.57 | 9.13/ 0.68 | 9.62/ 0.63 | 9.62/ 0.63 | 9.62/ 0.63 |
| Liner (µm) | | 150 | 100 | 150 | No | Yes | | 100 | No | No | Yes | Yes | Yes |
| Heat treatment | | SRA | SRA | SRA | stand. | stand. | | SRA | SRA | stand. | stand. | stand. | stand. |
| pressure (bar at RT) | | 40 | 40 | 40 | 30 | 6 | | 40 | 40 | 30 | 20 | 20 | 20 |

 = important test parameters

3



Figure 2 Tests carried out

ductility and ballooning, and the fill gas pressure as a test design parameter. This pressure will approximately double during test execution in response to the temperature increase in the system.

The tests have been used in several international code comparisons and benchmarking exercises. The commissioning tests number 1 and 2 were used for calibrating the codes to the conditions of the LOCA experiment system in the Halden Reactor.

2.3 How fuel fragmentation is observed

We have several ways to observe fuel fragmentation:

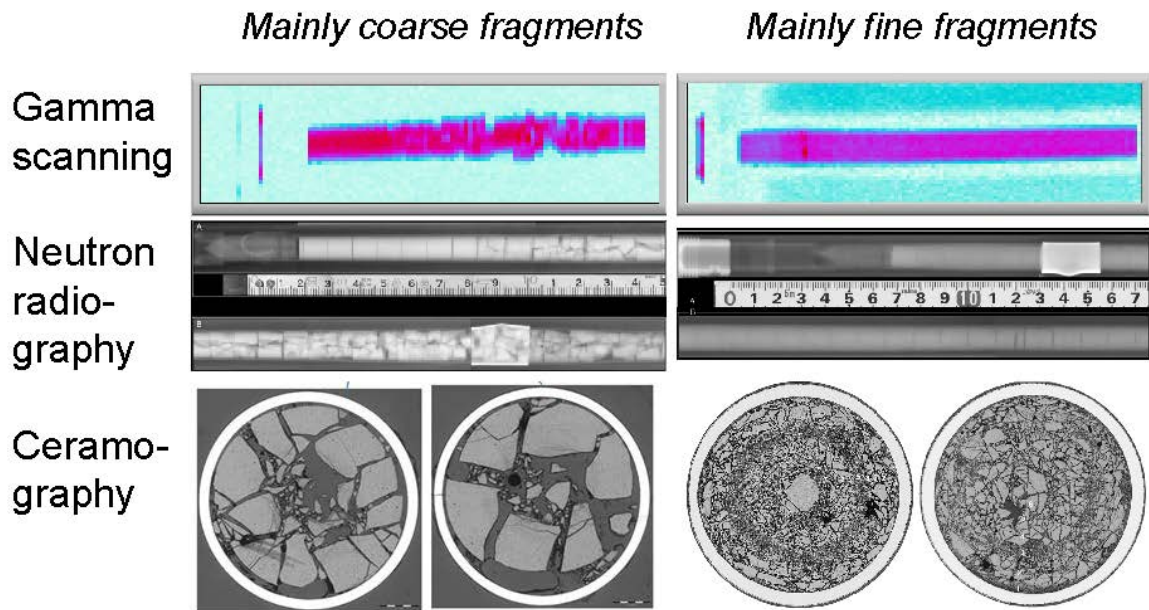
1. Gamma scanning

is carried out a few days after test execution. The test rig is slowly pulled out of the reactor and moved to a handling compartment in the reactor hall where the gamma scanning takes place. The fuel segment is kept vertical all the time in order to not change the fuel distribution in the cladding tube. The ragged appearance of the fuel column in the left gamma scan indicates coarse fragments which have moved laterally where ballooning has created some extra space. A small axial gap at the upper end indicates a little downward movement of the fuel column. The segments are from test 12 (left) and 5 (right).

The scan to the right shows no discernible structure and is an example of fine fragmentation and no lateral movement due to little ballooning.

3

How fuel fragmentation is observed



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Figure 3 Fuel fragmentation can be observed by gamma scanning, neutron radiography and ceramography

2. Neutron radiography

The next step is neutron radiography which is done a few months after test execution when the fuel has cooled sufficiently. The pictures show the same fuel as the gamma scanning. Neutron radiography reveals more details. In the left picture, it shows intact pellets and coarse fragments. In the right picture, one can see that the lower part of the segment must be strongly fragmented since pellet-pellet interfaces and dishings are not visible, while they are discernible in the upper part.







3. Ceramography

is the final examination. The ceramographs confirm the fragmentation deduced from gamma scanning and neutron radiography, but with much more detail at selected locations.

2.4 Neutron radiography details

This slide shows more examples of fragmentation as seen by neutron radiography. The pictures are arranged in order of increasing burnup. For the first four segments until 72 MWd/kg burnup, they show coarse fragments. This does not exclude the existence of fine fragments which cannot be seen with neutron radiography.

Neutron radiography details

| burnup, MWd/kg | 44.3 | 56 | 60 | 72.3 | 81.9 | 90 |
|------------------|---|---|---|--|---|---|
| radio- graphy |  |  |  |  |  |  |
| fragment size | coarse | coarse | coarse & some fine | coarse & fine | medium & fine | medium & fine |

5



Figure 4 Neutron radiography details

2.5 Fuel rim fragmentation

Irradiated fuel develops an outer rim of so-called high burnup structure. Ceramography reveals fragmentation of this rim structure fuel which increases with burnup. The first example with the lowest burnup shows some delamination of the rim structure fuel, but the fragments did not move. The third example with the highest burnup and thickest rim (calculated to be 1800 micro meter) shows very fine, relocated fragments. In comparison, the average width of a strand of human hair is about 100 micro meter.

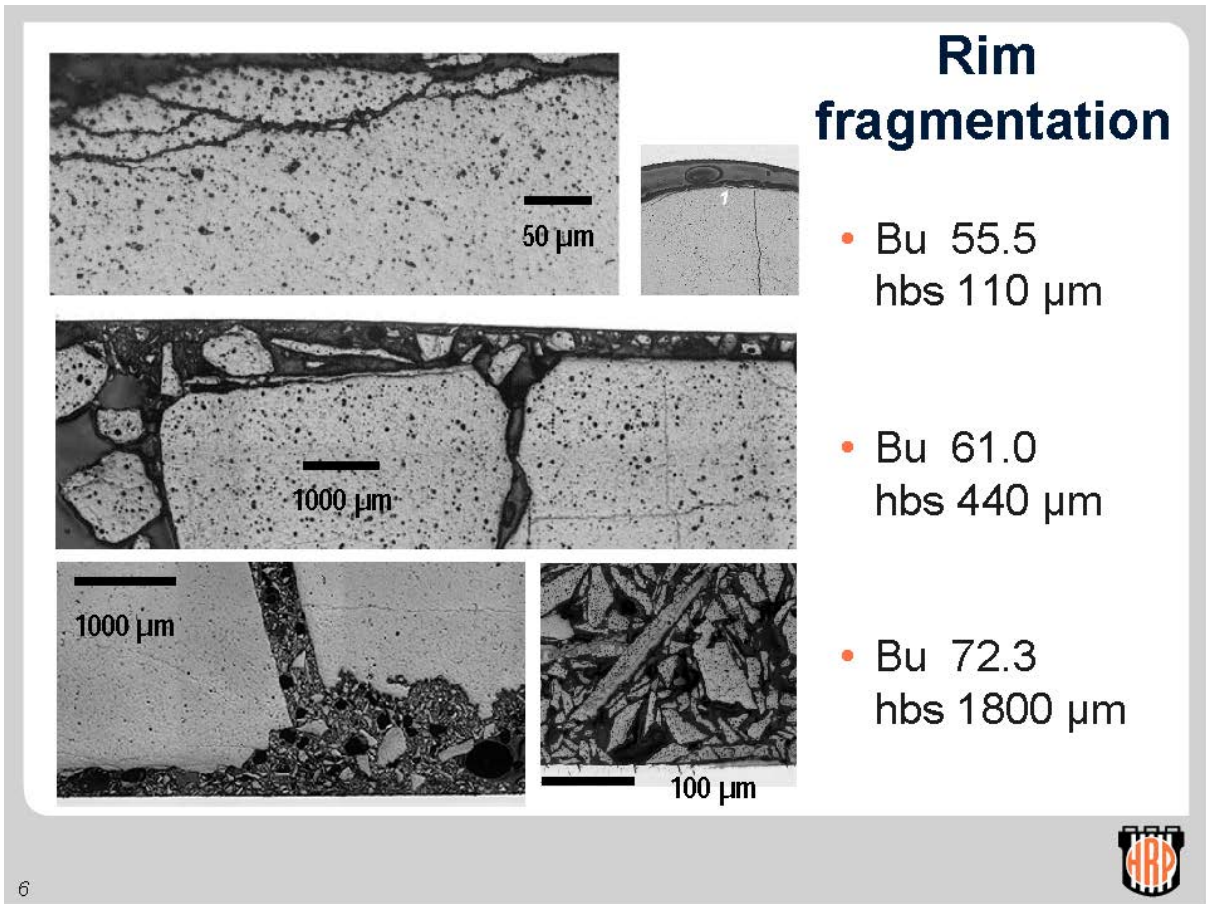


Fig. 5 Rim fragmentation

2.6 Cladding distension and fuel cracking

This slide tries to illustrate how cladding distension and fuel cracking are linked. Both segments, BWR fuel with similar burnup of about 72 MWd/kg, show coarse fragmentation in the vicinity of the ballooning where distension is strongest. Cracking decreases towards the lower end where the pellets still seem to be intact. The local cladding strain must exceed about 5% to produce visible fuel cracking and to allow fragment separation and movement.

The rotated, intact pellet at the lower end of IFA-650.13 had certainly enough free space around it to separate its fragments if they existed, but it did not do so. The distance to the burst location, from where a sudden pressure decrease propagates through the fuel stack on burst, may therefore play a role as well. Since distension is a function of distance to the burst location as well, the two possible influences on fragmentation would be correlated.

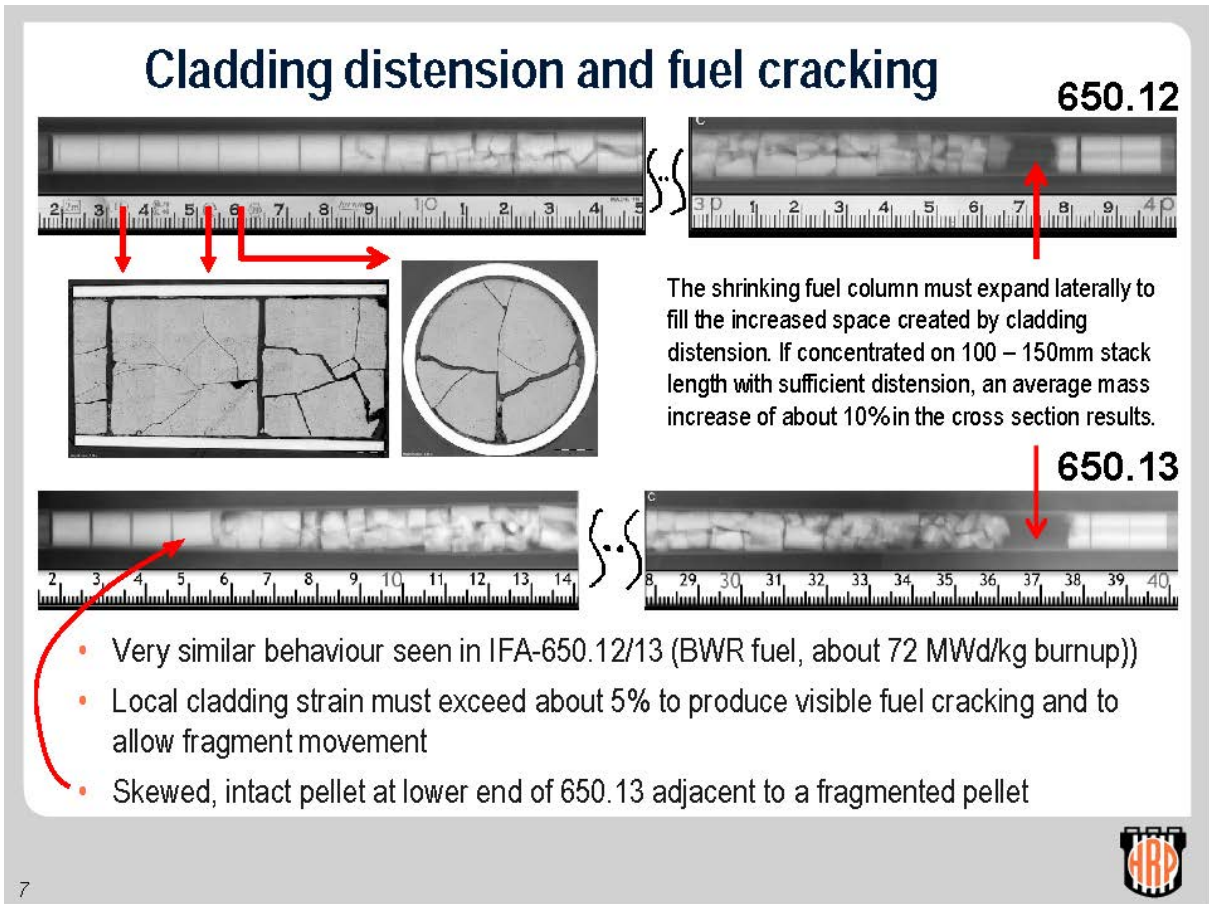


Figure 6 Cladding distension and fuel cracking

The upper end shows an axial gap of about 15mm in both cases. The shrinking fuel column must expand laterally to fill the increased space created by cladding distension. If concentrated on 100 – 150mm stack length with sufficient distension, an average mass increase of about 10% in the cross section would result.

2.7 Fuel fragmentation – summary

This slide summarises the evidence for fuel fragmentation presented in the previous slides. The qualitative impression is that up to a certain burnup, say 60 MWd/kg, fragmentation is more or less caused by the cracking during normal operation. The test segments with burnup of 72 MWd/kg and higher show additional fragmentation which progressively affects more and more of the pellet as burnup increases. The behaviour between 60 and 72 MWd/kg will be studied with the next test in the Halden reactor LOCA program.

Fuel fragmentation - summary

| test # | 2 | 7 | 6 | 11 | 10 | 12 | 13 | 3 | 5 | 9 | 4 |
|-------------------|--------|--------|--------|--------|--------------------------|------------------|------------------------------------|------------------|------------------|------------------|------------------|
| burnup, MWd/kg | 0 | 44.3 | 55.5 | 56 | 60 | 72.3 | 74.1 | 81.9 | 83 | 90 | 92 |
| balloon strain, % | 54 | 23 | 49 | 25 | 15 | 40 | 45 | 8 | 15 | 61 | 62 |
| radio- graphy | | | | | | | | | | | |
| ceramo- graphy | | | | | | | fragment size distribution only | | | | |
| fragment size | coarse | coarse | coarse | coarse | coarse & some fine | coarse & fine | coarse (& fine?) | medium & fine | medium & fine | medium & fine | medium & fine |

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Figure 7 Fuel fragmentation – summary

2.8 Fuel dispersal

If the fragments are small enough to pass through the burst opening, they can be dispersed driven by the rapid and strong outflow of gas when the cladding bursts. Evidence of dispersal can be seen in the gamma scanning pictures where a gamma signal coming from the bottom of the pressure flask indicates fuel that was expelled from the rod. Again, a correlation with burnup and the amount of high burnup structure is evident, but dispersal only happens for burnup above a threshold of about 60 MWd/kg.

Fuel dispersal

| test # | 2 | 7 | 6 | 11 | 10 | 12 | 13 | 3 | 5 | 9 | 4 |
|-------------------------------|--------|--------|--------|--------|--------------------|---------------|------------------|---------------|---------------|---------------|---------------|
| burnup, MWd/kg | 0 | 44.3 | 55.5 | 56 | 60 | 72.3 | 74.1 | 81.9 | 83 | 90 | 92 |
| balloon strain, % | 54 | 23 | 49 | 25 | 15 | 40 | 45 | 8 | 15 | 61 | 62 |
| balloon area, mm ² | 270 | 8 | ? | 1,5 | 38 | 1 | 10 | | 7 | 224 | 434 |
| fragment size | coarse | coarse | coarse | coarse | coarse & some fine | coarse & fine | coarse (& fine?) | medium & fine | medium & fine | medium & fine | medium & fine |
| gamma scan | | | | | | | | | | | |
| flask bottom → | | | | | | | | | | | |
| HBS width | | | | | | | | | | | |
| dispersal (qualitative) | none | none | none | none | some | some more | nearly none | | much | much more | much more |

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Figure 8 Fuel dispersal

2.9 Plans for HRP LOCA testing

The Halden Reactor Project plans for LOCA testing are defined as we go along. They are based on the results obtained so far and on input from

- Halden Reactor Project (HRP) members
- HRP Programme Group (technical steering group)

A LOCA workshop held in Lyon in 2012 identified, among others:

- Investigation of the effect of the spacer grid
- Rod length (or design which keeps the fuel in contact with the cladding for a certain length to see the effect of gas flow)
- Axial constraint

Plans for HRP LOCA testing

- Plans are defined as we go along. They are based on the results obtained so far and on input from
 - Halden Reactor Project (HRP) members
 - HRP Programme Group (technical steering group)
- A LOCA workshop, Lyon 2012, identified among others
 - Investigation of the effect of the spacer grid
 - Rod length (or design which keeps the fuel in contact with the cladding for a certain length to see the effect of gas flow)
 - Axial constraint

10



Figure 9 Plans for HRP LOCA testing









2.10 Next test

The HRP LOCA tests have shown that fuel fragmentation and dispersal are, among others, influenced by burnup. The burnup of the next test, 65 MWd/kgU, will be between test 10 which showed mostly coarse fragmentation and onset of fine fragmentation and test 12 which showed more fine fragmentation and more dispersal.

The peak clad temperature, PCT, will be 850 °C, and the fill gas pressure will be 40 bar. These conditions are the same as those of test 10 to which the next test will be compared.

Next test

- The HRP LOCA tests have shown that fuel fragmentation and dispersal are, among others, influenced by burnup
- The burnup of the next test, 65 MWd/kgU, will be between
 - test 10 which showed onset of fine fragmentation and
 - test 12 which showed more fine fragmentation and more dispersal
- PCT, pressure as for test 10

| | | | | |
|-------------------------|---|---|---|---|
| test # | 11 | 10 | 15 | 12 |
| burnup, MWd/kg | 56 | 60 | 65 | 72.3 |
| fragment size | coarse | coarse & some fine | ? | coarse & fine |
| gamma scan |  |  |  |  |
| flask bottom → |  |  |  |  |
| dispersal (qualitative) | none | some | ? | some more |

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Figure 10 Next test

2.11 Pressure drop

The test after the next one will probably address the influence of a phenomenon which was observed in three of the eleven tests with pre-irradiated fuel, namely a slow decrease of the pressure in the rod plenum after burst. This is shown in the plot which also contains an example of instantaneous pressure loss, curve labelled “4”. The graph to the right shows the post-LOCA cladding diameter of test IFA-650.5 and cross sections taken at positions with little and strong cladding distension. The difference in fragmentation is evident. The fuel maintained tight contact with the cladding along a certain length, and the cracking pattern depends on position.

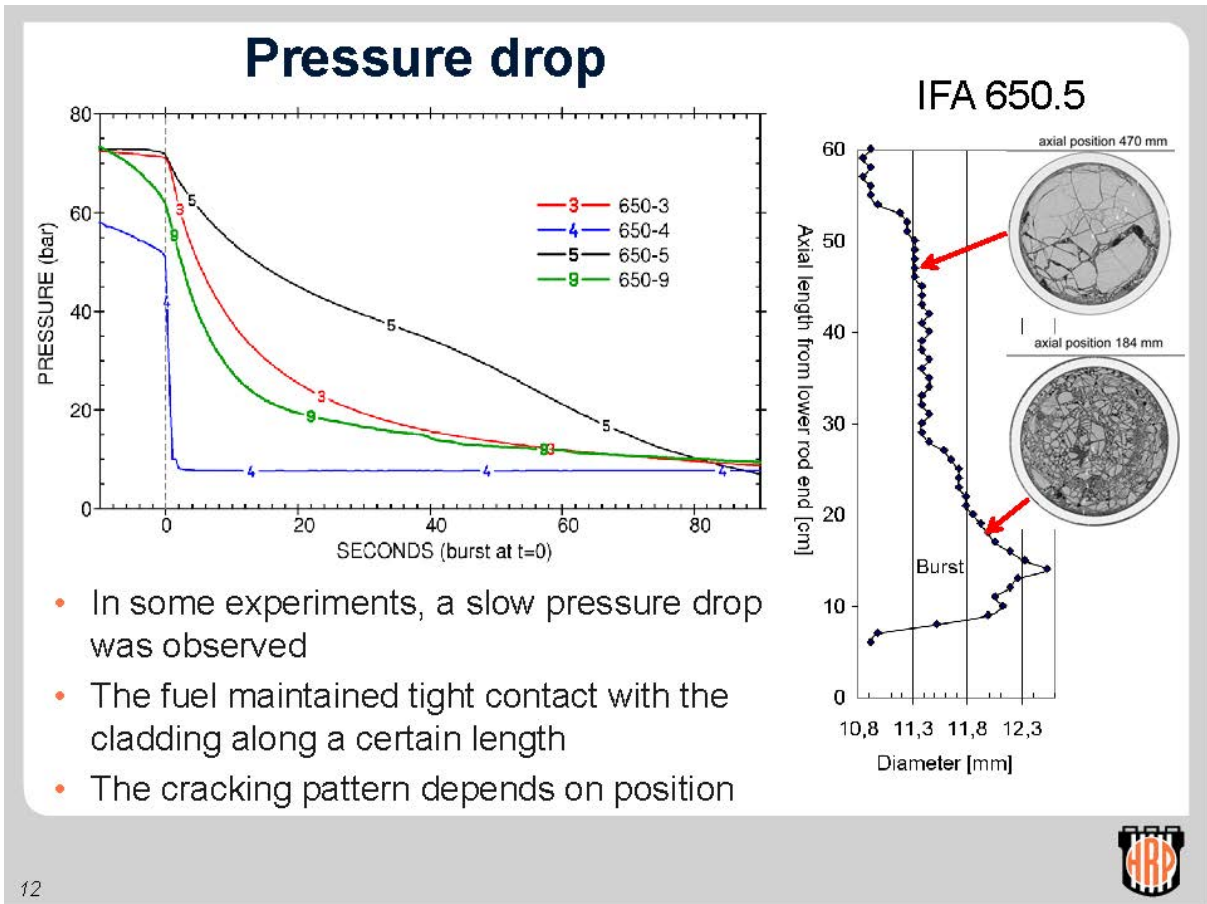


Figure 11 Pressure drop

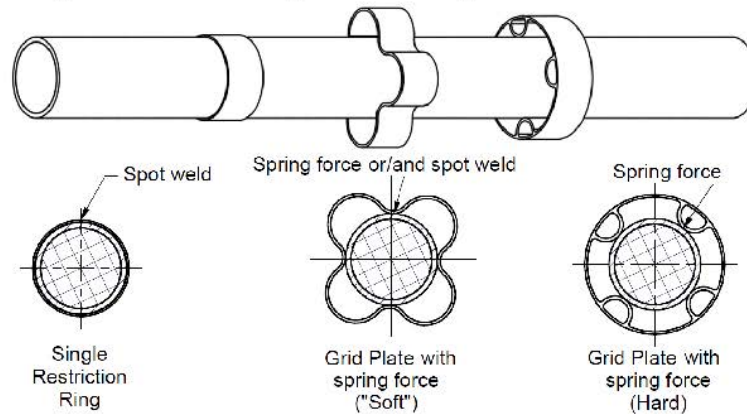
2.12 Test with spacer grid

The intention is then to determine the impact of a spacer element on axial gas transport, ballooning and fuel dispersal. The function of the spacer is both to provide a mechanical constraint and to influence local cooling, in this way decreasing cladding distension and impeding gas communication which possibly has an influence on fuel fragmentation and dispersal.

The shape of the grid is not decided. The example illustrates possible designs.

Test with spacer grid

- Determine the impact of a spacer element on axial gas transport, ballooning and fuel dispersal
- The function of the spacer is both to provide a mechanical constraint and to influence local cooling, in this way decreasing cladding distension



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Figure 12 Test with spacer grid

2.13 Acknowledgement

The OECD HRP LOCA test series IFA-650 is the result of the combined efforts of many contributors. Their contributions are gratefully acknowledged.

Acknowledgement

The OECD HRP LOCA test series IFA-650 is the result of the combined efforts of many contributors. The work of the following individuals is especially acknowledged:

Follow-up, evaluation and reporting

- Mikko Henrikki Pihlatie, Fortum, Finland
- Ville Lestinen, Fortum, Finland
- Mirkka Ek, Fortum, Finland
- Laura Kekkonen, VTT, Finland
- Radomír Jošek, NRI, Czech Republic
- Florian Bole du Chomont, EDF, France
- Alexandre Lavoil, EDF, France
- Olivier Bremond, EDF, France

Experiment preparation and execution

- Jon-Martin Karlsen
(design, refabrication and instrumentation)
- Erik Kolstad
(general preparation and guidance)
- Viktors Grismanovs, Boris Volkov
(test execution)
- Roar Suther (loop system)

Post-irradiation examination

- B. C. Oberländer, H. K. Jenssen, M. Espeland,
H. J. Kleemann, N. O. Solum, Juraj Balak

The efforts of the reactor crew in unloading the experiments, often under difficult conditions when the blow-down system was severely contaminated by ejected fuel, are gratefully acknowledged.

Special thanks go to VTT (Finland) and PSI (Switzerland) for supporting the test preparation and execution with pre-test calculations.



Figure 13 Acknowledgement

Appendix 1 Meeting agenda and picture

Agenda

| Topic | Speaker, Organization | Day | Time |
|--|-----------------------------|------------------|--------------------|
| 1. Welcome | RES/NRR Management | Thursday | 12:00 -12:15 |
| 2. Ground Rules and Meeting Logistics | Meeting Facilitator | | 12:15-12:30 |
| 3. Introduction and Meeting Objectives | T. Inverso, NRC | | 12:30-1:00 |
| 4. Research on Fuel Fragmentation, Relocation and Dispersal | - | | - |
| a. LOCA Experiments | - | | - |
| i. Fuel Fragmentation, Relocation and Dispersal Under LOCA Conditions: Experimental Observations | M. Flanagan, NRC | | 1:00-2:00 |
| ii. Fuel Fragmentation, Relocation and Dispersal, Current Understanding and Test Results | K. Yueh, EPRI | | 2:00-2:30 |
| <i>BREAK</i> | - | | <i>2:30-3:00</i> |
| iii. LOCA and fuel fragmentation tests in SCIP III | P. Askeljung, Studsvik | | 3:00-3:30 |
| iv. Overview of Halden Reactor LOCA experiments (with emphasis on fuel fragmentation) and plans | B. Oberlander, Halden | | 3:30-4:00 |
| v. Open Discussion* | ALL | 4:00-5:00 | |
| 5. Welcome and brief summary of Thursday's sessions | M. Flanagan, NRC | Friday | 9:00-9:15 |
| b. LOCA Analysis | - | | - |
| i. Methodology for Core-Wide Estimates of Fuel Dispersal During a LOCA | I. Porter & P. Raynaud, NRC | | 9:15-10:00 |
| ii. Analytical Assessment of High-Exposure Fuel Dispersal Potential During BWR LOCA | K. Muftuoglu, GEH | | 10:00-10:30 |
| iii. Assessment of Extent of Rupture in a Large Break LOCA | M. Nissley, Westinghouse | | 10:30-10:50 |
| i. Open Discussion* | ALL | | 10:50-11:15 |
| <i>BREAK</i> | - | | <i>11:15-11:30</i> |
| 6. Perspectives on Experiments and Analysis | | | |
| i. Potential Impacts on Design Basis Accidents | P. Clifford, NRC | | 11:30-12:00 |
| ii. IRSN views on fuel dispersion in RIA and LOCA accidents | M. Petit, IRSN | | 12:00-12:20 |
| iii. JAEA perspective on fuel fragmentation and dispersal | F. Nagase, JAEA | 12:20-12:40 | |
| iv. AREVA Perspective on Fuel Fragmentation and Dispersal During Design Basis Accidents | B. Dunn, AREVA | 12:40-1:00 | |
| <i>LUNCH</i> | - | <i>1:00-2:00</i> | |
| v. Open Discussion* | ALL | 2:00-2:30 | |
| 7. Summary and Conclusions, Next Steps | M. Flanagan, NRC | 2:30-3:00 | |

* Each agenda item includes time for 5-10 minutes of clarification-type questions immediately following each presentation. The designated open discussions are intended to provide time for in-depth discussion and public comment.



Mr. K. Yueh (EPRI), B. Oberländer (Halden Project,), Mr. P. Askeljung (Studsvik), M. Flanagan (US-NRC)